# C-A-2023 @ 2023 SIMPSON STRONG-TIE COMPANY INC.

# ET-3G™ Epoxy Adhesive



ET-3G is an epoxy-based, 1:1 ratio, two-component system ideal for general anchoring of threaded rod and rebar into concrete (cracked and uncracked) and masonry (cracked and uncracked).

#### **Features**

- Suitable for use under static and seismic loading conditions in cracked and uncracked concrete and masonry
- Ideal for general doweling and threaded rod applications
- Two-year shelf life for unopened cartridges stored between 45°F (7°C) and 90°F (32°C)

#### **Product Information**

Mix Ratio/Type	1:1 epoxy
Mixed Color	Teal
Base Materials	Concrete and masonry — cracked and uncracked
Base Material Conditions	Dry, water-saturated
Anchor Type	Threaded rod or rebar
Substrate Installation Temperature	50°F (4°C) to 110°F (43°C)
In-Service Temperature Range	-40°F (-40°C) to 150°F (65°C)
Storage Temperature	45°F (7°C) and 90°F (32°C)
Shelf Life	24 months
Volatile Organic Compound (VOC)	3 g/L
Chemical Resistance	See pp. 242–243
Manufactured in the US using global r	materials

#### **Test Criteria**

ET-3G has been tested in accordance with ICC-ES AC308, AC58, ACI 355.4 and applicable ASTM test methods.

#### Code Reports, Standards and Compliance

Concrete — ICC-ES ESR pending (including post-installed rebar connections, City of LA and Florida Building Code); FL15730.

Masonry — ICC-ES ESR pending.

ASTM C881 and AASHTO M235 - Types I/IV and II/V, Grade 3, Class C.

 $\mbox{UL Certification} - \mbox{CDPH Standard Method v1.2}.$ 

NSF/ANSI/CAN 61 (216 in. $^2$  / 1,000 gal.)

#### Installation Instructions

Installation instructions are located at the following locations: pp. 48–51; product packaging; or **strongtie.com/et3g**.

• Hole cleaning brushes are located on p. 52.

#### ET-3G Cartridge System

	Model No.	Capacity (ounces)	Cartridge Type	Carton Quantity	Dispensing Tool(s)	Mixing Nozzle <sup>3</sup>
<b></b>	ET3G10⁴	8.5	Single	12	CDT10S	
<b></b>	ET3G22-N⁴	22	Side-by-Side	-by-Side 10 EDT22S, EDTA22P, EDTA2		EMN22I
靊	ET3G56	56	Side-by-Side	6	EDTA56P	

- 1. Cartridge estimation guidelines are available at strongtie.com/softwareandwebapplications/category.
- 2. Detailed information on dispensing tools, mixing nozzles and other adhesive accessories is available at **strongtie.com**.
- 3. Use only Simpson Strong-Tie mixing nozzles in accordance with Simpson Strong-Tie instructions. Modification or improper use of mixing nozzle may impair ET-3G adhesive performance.
- 4. One EMN22I mixing nozzle and one nozzle extension are supplied with each cartridge.
- 5. Use of rodless pneumatic tools to dispense single-tube, coaxial adhesive cartridges is prohibited.



ET-3G Adhesive

# ET-3G™ Epoxy Adhesive

# SIMPSON Strong-Tie

#### ET-3G Cure Schedule

Base Materia	l Temperature	Gel Time	Cure Time
°F	°C	(minutes)	(hr.)
50	10	100	72
60	16	75	48
70	21	50	24
90	32	30	24
110	43	18	24

For water-saturated concrete, the cure times must be doubled.

#### ET-3G Typical Properties

	Promoute	Class C	Test
	Property	(>60°F)	Method
Consistency		Non-sag	ASTM C881
	Hardened to Hardened Concrete, 2-Day Cure <sup>1</sup>	2,600 psi	
Bond Strength, Slant Shear	Hardened to Hardened Concrete, 14-Day Cure <sup>1</sup>	2,900 psi	ASTM C882
	Fresh to Hardened Concrete, 14-Day Cure <sup>2</sup>	2,000 psi	
Compressive Yield Strength, 7-D	ay Cure <sup>1</sup>	13,000 psi	ASTM D695
Compressive Modulus, 7-Day Cu	ıre <sup>1</sup>	580,000 psi	ASTM D695
Heat Deflection Temperature, 7-	Day Cure <sup>2</sup>	132°F (56°C)	ASTM D648
Glass Transition Temperature, 7-	Day Cure <sup>2</sup>	124°F (51°C)	ASTM E1356
Decomposition Temperature, 24	-Hour Cure <sup>2</sup>	500°F (260°C)	ASTM E2550
Water Absorption, 24-Hours, 7-D	Day Cure <sup>2</sup>	0.15%	ASTM D570
Shore D Hardness, 24-Hour Cure	9 <sup>2</sup>	84	ASTM D2240
Linear Coefficient of Shrinkage,	7-Day Cure <sup>2</sup>	0.002 in./in.	ASTM D2566
Coefficient of Thermal Expansion	<sup>2</sup>	2.4 x 10 <sup>-5</sup> in./in.°F	ASTM C531

- 1. Material and curing conditions: 60° ± 2°F.
- 2. Material and curing conditions: 73°  $\pm$  2°F.

#### ET-3G Installation Information and Additional Data for Threaded Rod and Rebar<sup>1</sup>



Characteristic		Cumbal	Units	Nominal Anchor Diameter (in.) / Rebar Size								
Glididelelistic		Symbol	UIIILS	% / #3	1/2 / #4	% / #5	3/4 / #6	7⁄8 / # <b>7</b>	1 / #8	1¼/#10		
			Insta	llation Inform	ation							
Drill Bit Diameter		d <sub>hole</sub>	in.	1/2	5/8	3/4	7/8	1	11/8	1%		
Maximum Tightening Torque		T <sub>inst</sub>	ftlb.	10	20	30	45	60	80	125		
Permitted Embedment Depth Range	Minimum	h <sub>ef</sub>	in.	23/8	23/4	31/8	31/2	3¾	4	5		
remitted Embedment Depth Nange	Maximum	h <sub>ef</sub>	in.	71/2	10	12½	15	17½	20	25		
Minimum Concrete Thickness		h <sub>min</sub>	in.		$h_{ef}$ + 5 $d_{hole}$							
Critical Edge Distance <sup>2</sup>		Cac	in.				See footnote 2	2				
Minimum Edge Distance	C <sub>min</sub>	in.		23/4								
Minimum Anchor Spacing		S <sub>min</sub>	in.				3			6		

<sup>1.</sup> The information presented in this table is to be used in conjunction with the design criteria of ACI 318-19, ACI 318-14 and ACI 318-11.

 $[h/h_{ef}] \leq 2.4$ 

 $\tau_{\textit{k,uncr}} = \text{the characteristic bond strength in uncracked concrete, given in the tables that follow} \leq k_{\textit{uncr}} (\textit{(h}_{\textit{ef}} \times \textit{f'}_{\textit{c}})^{0.5} / (\pi \times \textit{d}_{\textit{hole}}))$ 

h = the member thickness (inches)

 $h_{ef}$  = the embedment depth (inches)

<sup>2.</sup>  $c_{ac} = h_{ef} (\tau_{k,uncr}/1,160)^{0.4} \times [3.1 - 0.7(h/h_{ef})]$ , where:

### ET-3G™ Design Information — Concrete



#### ET-3G Tension Strength Design Data for Threaded Rod<sup>1,11</sup>



							Nominal A	nchor Dia	meter (in.	)	
	Characteristic		Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	11/4
		Steel St	rength in T	ension	•		•	•			•
	Minimum Tensile Stress Area		Ase	in <sup>2</sup>	0.078	0.142	0.226	0.334	0.462	0.606	0.969
	Tension Resistance of Steel — ASTM F1554, G	Grade 36			4,525	8,235	13,110	19,370	26,795	35,150	56,200
	Tension Resistance of Steel — ASTM A193, Gr	rade B7			9,750	17,750	28,250	41,750	57,750	75,750	121,125
Threaded Rod	Tension Resistance of Steel — Type 410 Stainl (ASTM A193, Grade B6)	less	N <sub>sa</sub>	lb.	8,580	15,620	24,860	36,740	50,820	66,660	106,590
	Tension Resistance of Steel — Types 304 and (ASTM A193, Grade B8 and B8M)	316 Stainless			4,445	8,095	12,880	19,040	26,335	34,540	55,235
	Strength Reduction Factor — Steel Failure		φ	_			•	0.757			
	Concrete Brea	kout Strength i	n Tension (	2,500 p	si ≤ f' <sub>C</sub> ≤ 8	B,000 psi)	10				
Effectiveness F	actor — Uncracked Concrete		k <sub>uncr</sub>	_				24			
Effectiveness F	actor — Cracked Concrete		k <sub>cr</sub>	_				17			
Strength Reduc	tion Factor — Breakout Failure		φ	_				0.657			
	Bond St	trength in Tensi	on (2,500 p	osi ≤ f'c	≤ <b>8,000</b> p	osi)10					
	Characteristic Bond Strength <sup>5</sup>		$ au_{k,uncr}$	psi			See stror	ngtie.com	for values		
Uncracked Concrete 2,3,4	Permitted Embedment Depth Range	Minimum	h.	in.	2%	2¾	31/8	3½	3¾	4	5
		Maximum	h <sub>ef</sub>	111.	71/2	10	121/2	15	17½	20	25
	Characteristic Bond Strength <sup>5,8,9</sup>	Characteristic Bond Strength <sup>5,8,9</sup>		psi	See <b>strongtie.com</b> for values						
Cracked Concrete 2,3,4	Permitted Embedment Depth Range	Minimum	h .	in.	3	4	5	6	7	8	10
	Permitted Embedment Deptir Nange	Maximum	- h <sub>ef</sub>	111.	71/2	10	12½	15	17½	20	25
	Bond Strength in Tension —	Bond Strength	Reduction	Factors	s for Conti	inuous Sp	ecial Insp	ection			
Strength Reduc	etion Factor — Dry Concrete		φ <sub>dry, ci</sub>	_	0.657						
Strength Reduc	tion Factor — Water-Saturated Concrete — $h_{ef} \le$	12d <sub>a</sub>	φ <sub>sat,ci</sub>		0.9	55 <sup>7</sup>			$0.45^{7}$		
Additional Factor	or for Water-Saturated Concrete — $h_{ef} \le 12d_a$		K <sub>sat,ci</sub> 6	_			1			0.	84
Strength Reduc	tion Factor — Water-Saturated Concrete — h <sub>ef</sub> >	> 12d <sub>a</sub>	φ <sub>sat,ci</sub>	_				0.457			
Additional Factor	or for Water-Saturated Concrete — $h_{ef} > 12d_a$		k <sub>sat,ci</sub> 6	_				0.57			
	Bond Strength in Tension –	– Bond Strengt	h Reductio	n Facto	rs for Per	iodic Spec	cial Inspec	tion			
Strength Reduc	tion Factor — Dry Concrete		φ <sub>dry,pi</sub>	_				0.557			
Strength Reduc	tion Factor — Water-Saturated Concrete — h <sub>ef</sub> <	12d <sub>a</sub>	φ <sub>sat,pi</sub>	_				0.457			
Additional Factor	or for Water-Saturated Concrete — h <sub>ef</sub> ≤ 12d <sub>a</sub>		K <sub>sat,pi</sub> 6	_		1		0.93		0.	71
Strength Reduc	ction Factor — Water-Saturated Concrete — h <sub>ef</sub> >	> 12d <sub>a</sub>	φ <sub>sat,pi</sub>	_				0.457			
Additional Factor	or for Water-Saturated Concrete — h <sub>ef</sub> > 12d <sub>a</sub>		K <sub>sat,pi</sub> 6	_				0.48			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-19, ACI 318-14 and ACI 318-11.
- 2. Temperature Range: Maximum short-term temperature = 150°F, Maximum long-term temperature = 110°F.
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term temperatures are roughly constant over significant periods of time.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be increased by 72%.
- 6. In water-saturated concrete, multiply  $\tau_{k,uncr}$  and  $\tau_{k,cr}$  by  $K_{sat}$ .
- 7. The tabulated value of  $\phi$  applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of  $\phi$ .
- 8. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for %" anchors must be multiplied by  $\alpha_{N,\text{Seis}} = 0.80$ .
- 9. For anchors installed in regions assigned to Seismic Design Category C, D, E or F, the bond strength values for 1" anchors must be multiplied by  $\alpha_{N,\text{seis}} = 0.92$ .
- 10. The values of f'<sub>c</sub> used for calculation purposes must not exceed 8,000 psi (55.1 MPa) for uncracked concrete. The value of f'<sub>c</sub> used for calculation purposes must not exceed 2,500 psi (17.2 MPa) for tension resistance in cracked concrete.
- 11. For lightweight concrete, the modification factor for bond strength shall be as given in ACI 318-19 17.2.4, ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable, where applicable.

# ET-3G™ Design Information — Concrete



#### ET-3G Tension Strength Design Data for Rebar<sup>1,9</sup>









	01 1 1 1				Rebar Size						
	Characteristic		Symbol	Units	#3	#4	#5	#6	#7	#8	#10
		Stee	el Strength in	Tension							•
	Minimum Tensile Stress Area		A <sub>se</sub>	in <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.23
Rebar	Tension Resistance of Steel — (ASTM A615 Grade 60)	- Rebar	N <sub>sa</sub>	lb.	9,900	18,000	27,900	39,600	54,000	71,100	110,700
	Strength Reduction Factor — S	Steel Failure	φ	_				0.657			
	Concrete B	reakout Stren	gth in Tension	(2,500 psi	$\leq f_{C}^{\prime} \leq 8$ ,	000 psi) <sup>8</sup>					
Effectiveness Factor — Uno	cracked Concrete		<i>k</i> <sub>uncr</sub>	_				24			
Effectiveness Factor — Cra	cked Concrete		<i>k</i> <sub>cr</sub>	_				17			
Strength Reduction Factor -	— Breakout Failure		φ	_				0.657			
	Bono	d Strength in 1	Tension (2,500	psi ≤ f' <sub>C</sub> ≤	8,000 ps	i) <sup>8</sup>					
		$\tau_{k,uncr}$	psi			See <b>stror</b>	ngtie.com	for values			
Uncracked Concrete <sup>2,3,4</sup>	Permitted Embedment Depth Range	Minimum	h <sub>ef</sub>	in.	2%	2¾	31/8	31/2	3¾	4	5
		Maximum			71/2	10	12½	15	17½	20	25
	Characteristic Bond Strength <sup>5</sup>	$ au_{k,cr}$	psi			See stror	ngtie.com	for values			
Cracked Concrete <sup>2,3,4</sup>	Permitted Embedment Depth Range	Minimum	h	in	3	4	5	6	7	8	10
		Maximum	h <sub>ef</sub>	in.	71/2	10	12½	15	171/2	20	25
	Bond Strength in Tension	— Bond Strer	ngth Reduction	n Factors f	or Continu	ous Spec	ial Inspec	ction			
Strength Reduction Factor -	— Dry Concrete		φ <sub>dry,ci</sub>	_				$0.65^{7}$			
Strength Reduction Factor -	— Water-Saturated Concrete – h <sub>ef</sub>	≤ 12d <sub>a</sub>	φ <sub>sat,ci</sub>	_	0.	55 <sup>7</sup>			0.457		
Additional Factor for Water-	Saturated Concrete $-h_{ef} \le 12d_a$		K <sub>sat,ci</sub> 6	_			1			0.	84
Strength Reduction Factor -	— Water-Saturated Concrete – h <sub>ef</sub>	> 12d <sub>a</sub>	φsat,ci	_				$0.45^{7}$			
Additional Factor for Water-	Saturated Concrete – h <sub>ef</sub> > 12d <sub>a</sub>		K <sub>sat,ci</sub> 6	_				0.57			
	Bond Strength in Tension	n — Bond Stre	ength Reducti	on Factors	for Perio	dic Specia	al Inspecti	ion			
Strength Reduction Factor -	— Dry Concrete		φ <sub>dry,pi</sub>	_				$0.55^{7}$			
Strength Reduction Factor -	— Water-Saturated Concrete – h <sub>ef</sub>	≤ 12d <sub>a</sub>	φ <sub>sat,pi</sub>	_				0.457			
Additional Factor for Water-	Saturated Concrete – h <sub>ef</sub> ≤ 12d <sub>a</sub>		K <sub>sat,pi</sub> 6	_		1		0.93		0.	71
Strength Reduction Factor -	— Water-Saturated Concrete – h <sub>ef</sub>	> 12d <sub>a</sub>	φ <sub>sat,pi</sub>	_				0.457			
Additional Factor for Water-	Saturated Concrete – h <sub>ef</sub> > 12d <sub>a</sub>		K <sub>sat,pl</sub> 6	_				0.48			

- 1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-19, ACI 318-14 and ACI 318-11.
- $2. Temperature \ {\it Range: Maximum short-term temperature = 150°F, Maximum long-term temperature = 110°F.}$
- 3. Short-term concrete temperatures are those that occur over short intervals (diurnal cycling).
- 4. Long-term temperatures are roughly constant over significant periods of time.
- 5. For anchors that only resist wind or seismic loads, bond strengths may be increased by 72%.
- 6. In water-saturated concrete, multiply  $\tau_{k,uncr}$  and  $\tau_{k,cr}$  by  $K_{sat}$ .
- 7. The tabulated value of  $\phi$  applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of  $\phi$ .
- 8. The values of  $f_c$  used for calculation purposes must not exceed 8,000 psi (55.1 MPa) for uncracked concrete. The value of  $f_c$  used for calculation purposes must not exceed 2,500 psi (17.2 MPa) for tension resistance in cracked concrete.
- For lightweight concrete, the modification factor for bond strength shall be as given in ACI 318-19 17.2.4, ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable, where applicable.

# **ET-3G**<sup>™</sup> Design Information — Concrete

#### ET-3G Shear Strength Design Data for Threaded Rod<sup>1</sup>

	Characteristic		Units	Nominal Anchor Diameter (in.)							
	Glaracteristic	Symbol	Oiiito	3/8	1/2	5/8	3/4	7/8	1	11/4	
	Steel	Strength	in Shea	ır					'		
	Minimum Shear Stress Area	A <sub>se</sub>	in.²	0.078	0.142	0.226	0.334	0.462	0.606	0.969	
	Shear Resistance of Steel — ASTM F1554, Grade 36			2,260	4,940	7,865	11,625	16,080	21,090	33,720	
	Shear Resistance of Steel — ASTM A193, Grade B7			4,875	10,650	16,950	25,050	34,650	45,450	72,675	
Threaded Rod	Shear Resistance of Steel — Type 410 Stainless (ASTM A193, Grade B6)	V <sub>sa</sub>	lb.	4,290	9,370	14,910	22,040	30,490	40,000	63,955	
	Shear Resistance of Steel — Types 304 and 316 Stainless (ASTM A193, Grade B8 & B8M)			2,225	4,855	7,730	11,420	15,800	20,725	33,140	
Hou	Reduction for Seismic Shear — ASTM F1554, Grade 36			0.87	0.78		0.	68		0.65	
	Reduction for Seismic Shear — ASTM A193, Grade B7			0.87	0.78		0.	68		0.65	
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B6)	$\alpha_{V,seis}^3$	_	0.69	0.82	0.75 0.83			0.83	0.72	
	Reduction for Seismic Shear — Stainless (ASTM A193, Grade B8 & B8M)			0.69	0.82		0.75		0.83	0.72	
	Strength Reduction Factor — Steel Failure	φ	_	$0.65^{2}$							
	Concrete Br	eakout S	trength i	in Shear							
Outside D	iameter of Anchor	d <sub>o</sub>	in.	0.375	0.5	0.625	0.75	0.875	1	1.25	
Load Bear	ring Length of Anchor in Shear	$\ell_e$	in.		Mir	n. of <i>h<sub>ef</sub></i> and	d 8 times a	nchor diam	eter		
Strength F	Reduction Factor — Breakout Failure	φ	_				0.702				
	Concrete F	ryout Str	ength in	Shear							
Coefficien	t for Pryout Strength	k <sub>cp</sub>	_		1.0	o for $h_{ef} < 2$	2.50"; 2.0 1	for $h_{ef} \ge 2.5$	50"		
Strength F	Reduction Factor — Pryout Failure	φ	_				0.702				

<sup>1.</sup> The information presented in this table is to be used in conjunction with the design criteria of ACI 318-19, ACI 318-14 and ACI 318-11.

<sup>2.</sup> The tabulated value of  $\phi$  applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of  $\phi$ .

<sup>3.</sup> The values of  $V_{sa}$  are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F,  $V_{sa}$  must be multiplied by  $\alpha_{V,seis}$  for the corresponding anchor steel type.

#### **ET-3G**<sup>™</sup> Design Information Concrete



#### ET-3G Shear Strength Design Data for Rebar<sup>1</sup>









	Characteristic	Cumbal	Units	Rebar Size							
	Gilai delei isule	Symbol	UIIILS	#3	#4	#5	#6	#7	#8	#10	
	:	Steel Strenç	yth in Shear	r							
	Minimum Shear Stress Area		in <sup>2</sup>	0.11	0.2	0.31	0.44	0.6	0.79	1.23	
Rebar	Shear Resistance of Steel — Rebar (ASTM A615 Grade 60)	V <sub>sa</sub>	lb.	4,950	10,800	16,740	23,760	32,400	42,660	66,420	
nebai	Reduction for Seismic Shear — Rebar (ASTM A615 Grade 60)	$\alpha_{V,seis}$ <sup>3</sup>	_	0.85	0.88	0.	84	0.	77	0.59	
	Strength Reduction Factor — Steel Failure	φ	_	- 0.60 <sup>2</sup>							
	Concre	te Breakout	Strength in	n Shear							
Outsid	e Diameter of Anchor	$d_0$	in.	0.375	0.5	0.625	0.75	0.875	1	1.25	
Load-E	Bearing Length of Anchor in Shear	$\ell_e$	in.		Mir	i. of <i>h<sub>ef</sub></i> and	d 8 times a	nchor diam	eter		
Streng	th Reduction Factor — Breakout Failure	φ	_				$0.70^{2}$				
	Concr	ete Pryout	Strength in	Shear							
Coeffic	cient for Pryout Strength	K <sub>cp</sub>	_		1.0	) for $h_{ef} < 2$	2.50"; 2.0 1	for $h_{ef} \ge 2.5$	50"		
Streng	th Reduction Factor — Pryout Failure	φ	_				0.702				

<sup>1.</sup> The information presented in this table is to be used in conjunction with the design criteria of ACI 318-19, ACI 318-14 and ACI 318-11.

For additional load tables, visit strongtie.com/et3g.



## **Adhesive Cartridge Estimator**

Simpson Strong-Tie® Adhesive Cartirdge Estimator software will help you easily estimate how much adhesive you will need for your project, including threaded rod and rebar doweling, and crack injection.

<sup>2.</sup> The tabulated value of ∮ applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, refer to ACI 318-11 D.4.4 to determine the appropriate value of  $\phi$ .

<sup>3.</sup> The values of  $V_{sa}$  are applicable for both cracked concrete and uncracked concrete. For anchors installed in regions assigned to Seismic Design Category C, D, E or F,  $V_{sa}$  must be multiplied by  $\alpha_{V,seis}$ .

#### ET-3G™ Design Information -- Concrete



#### ET-3G Development Length for Rebar Dowels







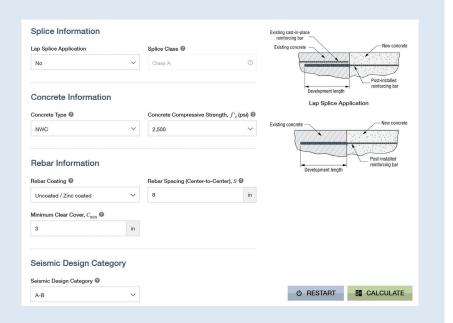


			Development Length, in. (mm)								
Rebar Size	Drill Bit Diameter (in.)	Clear Cover in. (mm)	f' <sub>c</sub> = 2,500 psi (17.2 MPa) Concrete	f' <sub>c</sub> = 3,000 psi (20.7 MPa) Concrete	f' <sub>c</sub> = 4,000 psi (27.6 MPa) Concrete	f' <sub>c</sub> = 6,000 psi (41.4 MPa) Concrete	f' <sub>c</sub> = 8,000 psi (55.2 MPa) Concrete				
<b>#3</b> (9.5)	1/2	<b>1½</b> (38)	<b>12</b> (305)								
<b>#4</b> (12.7)	5%	<b>1½</b> (38)	<b>14.4</b> (366)	<b>14</b> (356)	<b>12</b> (305)	<b>12</b> (305)	<b>12</b> (305)				
<b>#5</b> (15.9)	3/4	1½ (38)	<b>18</b> (457)	<b>17</b> (432)	<b>14.2</b> (361)	<b>12</b> (305)	<b>12</b> (305)				
<b>#6</b> (19.1)	7/8	<b>1½</b> (38)	<b>21.6</b> (549)	<b>20</b> (508)	<b>17.1</b> (434)	<b>14</b> (356)	<b>13</b> (330)				
<b>#7</b> (22.2)	1	<b>3</b> (76)	<b>31.5</b> (800)	<b>29</b> (737)	<b>25</b> (635)	<b>21</b> (533)	<b>18</b> (457)				
<b>#8</b> (25.4)	11/8	<b>3</b> (76)	<b>36</b> (914)	<b>33</b> (838)	<b>28.5</b> (724)	<b>24</b> (610)	<b>21</b> (533)				
<b>#9</b> (28.7)	1%	<b>3</b> (76)	<b>40.5</b> (1,029)	<b>38</b> (965)	<b>32</b> (813)	<b>27</b> (686)	<b>23</b> (584)				
<b>#10</b> (32.3)	1%	<b>3</b> (76)	<b>45</b> (1,143)	<b>42</b> (1,067)	<b>35.6</b> (904)	<b>30</b> (762)	<b>26</b> (660)				
<b>#11</b> (35.8)	13/4	<b>3</b> (76)	<b>51</b> (1,295)	<b>47</b> (1,194)	<b>41</b> (1,041)	<b>33</b> (838)	<b>29</b> (737)				

- 1. Tabulated development lengths are for static, wind and seismic load cases in Seismic Design Category A and B. Development lengths in SDC C through F must comply with ACI 318-19 and ACI 318-14 Chapter 18 or ACI 318-11 Chapter 12, as applicable. The value of f'c used to calculate development lengths shall not exceed 2,500 psi in SDC C through F.
- 2. Rebar is assumed to be ASTM A615 Grade 60 or A706 ( $f_y = 60,000$  psi). For rebar with a higher yield strength, multiply tabulated values by  $f_y$  / 60,000 psi.
- 3. Concrete is assumed to be normal-weight concrete. For lightweight concrete, multiply tabulated values by 1.33.
- 4. Tabulated values assume bottom cover of less than 12" cast below rebars ( $\Psi_t$  = 1.0).
- 5. Uncoated repar must be used
- 6. The value of  $K_{tr}$  is assumed to be 0. Refer to ACI 318-19 Section 25.4.2.4, ACI 318-14 Section 25.4.2.3 or ACI 318-11 Section 12.2.3.

# Rebar **Development** Length **Calculator**

Rebar Development Length Calculator is a web application that supports the design of post-installed rebar in concrete applications by calculating the necessary tension and compression development lengths required in accordance with ACI 318-19 / ACI 318-14.



# Masonry

ET-3G Epoxy Anchor Installation Information — Fully Grouted CMU Construction — Face of Wall

Installation Information	Cumbal	Units	Nominal Rod Diameter / Rebar Size							
instaliation illiorniation	Symbol	Units	%" / #3	1⁄2" / #4	5%" / #5	34" / #6				
Drill Bit Diameter — Threaded Rod	d <sub>o</sub>	in.	7/16	9/16	11/16	7/8				
Drill Bit Diameter — Rebar	d <sub>o</sub>	in.	1/2	5/8	3/4	7/8				
Minimum Embedment Depth	h <sub>ef,min</sub>	in.	3	3	3	3				

ET-3G Epoxy Anchor Installation Information — Fully Grouted CMU Construction — Top of Wall



Installation Information	Symbol	Units	Nominal Rod Diameter / Rebar Size		
			1⁄2" / #4	%" / #5	7∕8"
Drill Bit Diameter — Threaded Rod	$d_{o}$	in.	9/16	11/16	1
Drill Bit Diameter — Rebar	d <sub>o</sub>	in.	5/8	3/4	_
Minimum Embedment Depth	h <sub>ef,min</sub>	in.	3	3	3

ET-3G Epoxy Anchor Installation Information — Ungrouted CMU Construction



Installation Information	Symbol	Units	Nominal Rod Diameter		
			3%"	1/2"	5/8"
Drill Bit Diameter	d <sub>o</sub>	in.	9/16	3/4	7/8
Embedment Depth	h <sub>ef,min</sub>	in.	3½	3½	3½

Please see the ET-3G product page at strongtie.com and ICC-ES ESR Report for load data.